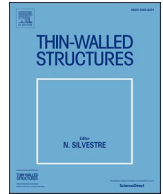




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Corrigendum to “Numerical analysis of axially loaded circular high strength concrete-filled double steel tubular short columns” [Thin-Walled. Struct. 138 (2019) 105–116]

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The authors regret that the above article contained some typewriting and calculation errors. The corrections are given as follows:

Page 115, in Section 8, the word ‘suing’ should read as ‘using’.

Page 115, the mean calculated-to-measured ultimate axial strengths calculated by using Eurocode 4 should read as 1.05.

Page 116, in Conclusion, Point 6, it should read as ‘the design rules specified by Eurocode 4 provides unconservative estimations’.

Page 110, in Table 2, the ultimate strengths ($P_{u,EC4}$) computed by using Eurocode 4 are corrected as follows:

Table 2 Ultimate axial strengths of circular CFDST short columns.

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Specimen	$P_{u,exp}$ (kN)	$P_{u,num}$ (kN)	$P_{u,EC4}$ (kN)	$P_{u,ACI}$ (kN)	$P_{u,AISC}$ (kN)	$P_{u,des}$ (kN)	$\frac{P_{u,num}}{P_{u,exp}}$	$\frac{P_{u,EC4}}{P_{u,exp}}$	$\frac{P_{u,ACI}}{P_{u,exp}}$	$\frac{P_{u,AISC}}{P_{u,exp}}$	$\frac{P_{u,des}}{P_{u,exp}}$
C1-1	1942	1818	1847	1407	1455	1823	0.94	0.95	0.72	0.75	0.94
C1-2	1911	1818	1846	1407	1455	1823	0.95	0.97	0.74	0.76	0.95
C2-1	1683	1409	1546	1196	1249	1425	0.84	0.92	0.71	0.74	0.85
C2-2	1592	1409	1546	1196	1249	1425	0.89	0.97	0.75	0.78	0.90
C2-3	1831	1730	1852	1470	1544	1781	0.94	1.01	0.80	0.84	0.97
C2-4	1875	1694	1811	1442	1516	1718	0.90	0.97	0.77	0.81	0.92
C2-5	1870	1813	1916	1532	1612	1837	0.97	1.02	0.82	0.86	0.98
C2-6	1925	1831	1908	1524	1605	1853	0.95	0.99	0.79	0.83	0.96
C3-1	1434	1214	1327	1042	1097	1231	0.85	0.93	0.73	0.77	0.86
C3-2	1425	1190	1303	1026	1080	1204	0.84	0.91	0.72	0.76	0.84
C4-1	1432	1276	1285	979	1009	1281	0.89	0.90	0.68	0.70	0.89
C4-2	1106	931	1041	810	842	948	0.84	0.94	0.73	0.76	0.86
C5-1	1256	1110	1149	883	915	1121	0.88	0.92	0.70	0.73	0.89
C5-2	1182	1110	1156	888	920	1126	0.94	0.98	0.75	0.78	0.95
S3-1-1	3626	4051	4305	3207	3351	3790	1.12	1.19	0.88	0.92	1.05
S3-1-2	8529	7834	7925	6467	6938	8022	0.92	0.93	0.76	0.81	0.94
S3-1-3	4968	4950	5262	4091	4323	5014	1.00	1.06	0.82	0.87	1.01
S3-1-4	5239	5175	5403	4220	4465	5193	0.99	1.03	0.81	0.85	0.99
S3-2-1	6300	6558	6378	4670	4783	5918	1.04	1.01	0.74	0.76	0.94
S3-2-2	9817	8943	9480	7526	7930	9211	0.91	0.97	0.77	0.81	0.94
S3-2-3	7022	6798	7222	5466	5660	6897	0.97	1.03	0.78	0.81	0.98
S3-2-4	7160	6794	7347	5583	5788	7041	0.95	1.03	0.78	0.81	0.98
A1-1	8142	8804	9542	6756	7043	7410	1.08	1.17	0.83	0.87	0.91
A2-1	9830	9079	9977	7057	7341	7720	0.91	1.00	0.71	0.74	0.78
A1-2	9830	9383	9992	7227	7506	7956	0.95	1.02	0.74	0.76	0.81
A2-2	10025	10189	11077	7947	8216	8586	1.02	1.10	0.79	0.82	0.86
A1-3	9740	9767	10244	7542	7818	8275	1.00	1.05	0.77	0.80	0.85
A2-3	10739	10801	11285	8222	8488	8755	1.01	1.05	0.77	0.79	0.82
CC1-SC1-OT1	1435.05	1460	1845	1247	1282	1429	1.02	1.29	0.87	0.89	1.00
CC1-SC1-OT2	1977.94	2090	2303	1605	1635	1972	1.06	1.16	0.81	0.83	1.00
CC1-SC2-OT1	1606.89	1673	1985	1412	1475	1661	1.04	1.23	0.88	0.92	1.03
CC1-SC2-OT2	2044.44	2278	2538	1817	1871	2237	1.11	1.24	0.89	0.92	1.09
CC2-SC1-OT1	1570.15	1627	1889	1328	1381	1563	1.04	1.20	0.85	0.88	1.00
CC2-SC1-OT2	2153.11	2255	2480	1767	1815	2182	1.05	1.15	0.82	0.84	1.01
CC2-SC2-OT1	1784.39	1839	2163	1574	1655	1877	1.03	1.21	0.88	0.93	1.05
CC2-SC2-OT2	2274.77	2374	2716	1979	2051	2448	1.04	1.19	0.87	0.90	1.08
DC-09	7640	7346	7875	6309	6727	7504	0.96	1.03	0.83	0.88	0.98
DC-10	7209	7699	8232	6629	7078	7878	1.07	1.14	0.92	0.98	1.09
DC-11	6882	6961	7490	5963	6346	7100	1.01	1.09	0.87	0.92	1.03
DC-12	8375	7699	8202	6602	7049	7847	0.92	0.98	0.79	0.84	0.94
Mean							0.97	1.05	0.79	0.83	0.95
Standard Deviation (SD)							0.08	0.11	0.06	0.07	0.08
Coefficients of Variance (CoV)							0.08	0.10	0.08	0.08	0.08